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## **AMENDMENTS TO THE SPECIFICATION**

Page 1, amend paragraph 2 to read:

Most ef loads in <u>a</u> distribution power system have the characteristic of inductance, and it will result in the <u>a</u> poor power factor. Hence, it requires a larger current for the identical real power that reduces the power efficiency of the distribution power system and degrades the performance of voltage regulation of the load side. For solving the above problems, power substations and power consumers generally install a passive type reactive power compensator (AC power capacitors) parallel connected to the distribution power system, so as to compensate a lagging reactive power to increase the entire power factor. In some distribution power system systems, the capacity of applied AC power eapacitor capacitors is about 25% to 35% of total capacity, and in some other distribution power system even exceeds about 50%, according to research reports.

Page 2, amend the first full paragraph to read:

Recently, harmonic pollution of industrial power system is <u>has</u> increased seriously due to the wide use of nonlinear loads. The AC power capacitor for power factor correction provides with a low impedance path for harmonic current, hence, the AC power capacitor is frequently damaged by harmonics. Meanwhile, it results in the power resonance between the AC power capacitor and the distribution power system. Then, it will result in A further result is the amplification of harmonic current and harmonic voltage. Thus, the destruction of the AC power capacitor due to over-voltage or over-current may occur. Besides, the over-voltage of AC power capacitor caused by the power resonance may destroy neighboring electric power facilities and even result in public accidents.

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Page 3, amend the first full paragraph to read:

There is another solution that wherein the AC power capacitor is switched off

from the power system when over-voltage or over-current occurs, but the function of

reactive power compensation will be failed.

Page 3, amend paragraph 2 to read:

The reactive power compensation also can be obtained by using a set of

constant AC power capacitors merely providing a fixed reactive power. This fixed

reactive power cannot be adjusted to respond to the variation of loads, and it may result

in over-voltage due to the a light load. In order to properly adjust reactive power

provided by the AC power capacitor, an automatic power factor regulator (APFR) is

developed, as shown in FIG. 1. The APFR is consisted consists of a set of AC power

capacitors C, through CN via switches S, through SN. Thereby the reactive power

supplied from the APFR can be adjusted by changing number of AC power capacitors

switching switched on. Although APFR can supply an adjustable reactive power to

respond to the variation of loads, the APFR can merely be adjusted step by step not

linearly. Therefore, the power factor of the distribution power system compensated by

APFR still cannot be close unity.

Page 4, amend paragraph 1 to read:

Referring to FIG. 2, another power factor regulator uses a fixed capacitor

parallel connected to a controllable reactor 1 l, which is controlled by a thyristor switch

10. This power factor regulator, so-called a Fixed Capacitor Thyristor-Controlled

Reactor (FC-TCR), uses a phase control technique to control the thyristor switch 10,

thereby whereby it can provide with a linearly adjustable reactive power. However, it

generates a significant amount of harmonic current and results in serious harmonic

pollution due to the use of the phase control technique in the thyristor.

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# Page 4, amend paragraph 3 to read:

Referring to FIG. 3, it-illustrates a facility based on power electronic technology to be applied in a distribution power system to compensate reactive power, so-called the active type reactive power compensator 2, is shown. This active type reactive power compensator uses a power converter 20 via an inductor 21 to be connected to a power system 1. The power converter 20 is connected to a DC power capacitor 22 at its DC side. The active type reactive power compensator 2 may provide with a leading reactive power or a lagging reactive power. The supplied reactive power can be adjusted linearly to respond to the variation of loads so that the input power factor can be maintained to be close to unity. Meanwhile, the active power factor correction system will not result in power resonance. Hence, it can avoid the destruction of the power resonance generated by an AC power capacitor. However, the active type reactive power compensator 2 must compensate the reactive power required by the loads, thus it requires a large capacity of power converter in the active type reactive power compensator. Hence, the wide application is limited due to the high cost.

### Page 5, amend the first full paragraph to read:

The present invention intends to provide a hybrid reactive power compensation device used for supplying the linearly adjustable reactive power within a predetermined range. Meanwhile, the hybrid reactive power compensation device includes an active type reactive power compensator to adjust a current flowing through a passive type reactive power compensator to be approximated as a sinusoidal waveform, and thereby it can avoid the power resonance generated between the hybrid reactive power compensation device and the reactance of power system. Therefore, it can avoid the destruction of hybrid reactive power compensation device itself and the neighboring power facilities by the power resonance. Moreover, the manufacture cost of the present invention is less expensive than that of the conventional active type reactive power compensator.

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## Page 6, amend paragraph 1 to read:

The primary objective of this invention is to provide a hybrid reactive power compensation device including a passive type reactive power compensator and an active type reactive power compensator serially connected thereto, which <u>is</u> adapted to supply a linearly adjustable reactive power and thereby avoid the destruction of power resonance. The manufacture cost of this invention is less expensive than that of the conventional active type reactive power compensator.

#### Page 6, amend paragraph 2 to read:

The hybrid reactive power compensation device in accordance with the present invention mainly comprises a passive type reactive power compensator and an active type reactive power compensator serially connected thereto. The passive type reactive power compensator is an AC power capacitor adapted to provide with reactive power that, thus, reduces reactive power supplied from the active type reactive power compensator. Additionally, it can reduce the voltage rating and the capacity of active type reactive power compensator. Since the cost of AC power capacitor is less expensive significantly than that of the active type reactive power compensator, the manufacture cost of the present invention is also less expensive than that of the conventional active type reactive power compensator. The active type reactive power compensator is consisted of comprises a power converter, a DC capacitor, a highfrequency ripple filter and a controller. The hybrid reactive power compensation device is adapted to supply linearly adjustable reactive power within a predetermined range. The hybrid reactive power compensation device can supply a current with a nearly sinusoidal waveform for reactive power compensation due to the use of active type reactive power compensator, and thereby it can avoid the power resonance generated by itself and reactance of the power system. Therefore, it can avoid the destruction of the hybrid reactive power compensator device itself and neighboring power facilities due to the power resonance.

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Page 9, amend paragraph 1 (bridging pages 9 and 10) to read:

FIG. 5 illustrates a block diagram of the controller 323 of the active type reactive power compensator 32 in accordance with the first embodiment of the present invention. The active type reactive power compensator 32 adopts is voltage control manner and the principle is controlled in a manner and principle as follows,

Assuming that the voltage of the power system 1 is

$$V_{S} = V_{S} \sin \omega t \tag{1}$$

Page 11, amend the first full paragraph to read:

Like the harmonic voltage (V<sub>h</sub>) contained in the power system 1, the active type reactive power compensator 32 is adapted to supply a harmonic voltage which has the magnitude and phase equivalent to those of the power system 1. Consequently, the voltage of the passive type reactive power compensator 31 is supplied with a sinusoidal waveform only contained a containing fundamental components to thereby avoid the power resonance generated by itself and reactance of the power system 1.

#### Page 11, amend paragraph 2 to read:

The present invention accomplishes to reduce the capacitance of the active type reactive power compensator 32 by means of the passive passive type reactive power compensator 31 providing with a reactive power. Moreover, the active type reactive power compensator 32 is able to adjust the reactive power supplied from the hybrid reactive power compensation device 3 in linear linearly within a predetermined range. Consequently, the active type reactive power compensator 32 is provided with a voltage equivalent to the harmonic voltage of the power system 1 so that the passive type reactive power compensator 31 can supply a current with a nearly sinusoidal waveform. Thereby, it can avoid resulting in the resonance destruction between the hybrid reactive power compensation device 3

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and the power system, and provide with a reliable reactive power of the passive type

reactive power compensator 31 and the active type reactive power compensator 32.

Page 12, amend the first full paragraph to read:

Referring again to FIGS. 4 and 5, the active type reactive power compensator

32 includes a controller 323. The active type reactive power compensator 32 adopts the

voltage mode control and a modulation signal for controlling the active type reactive

power compensator 32 can be obtained by adding three (first, second, and third) voltage

control signals  $(V_1, V_2 \text{ and } V_3)$ .

Page 12, amend paragraph 2 to read:

Referring again to FIGS. 4 and 5, the first voltage control signal V<sub>1</sub> is adapted

to adjust the reactive power in linear linearly for tuning. The fundamental wave equal

to the voltage of the power system 1 can be calculated by using Eq. (2). The load

current is sent to the first band-pass filter 500 to obtain its fundamental component, and

the voltage of power system is sent to the second band-pass filter 501 to obtain its

fundamental component. Then, both outputs of the first band-pass filter 500 and the

second band-pass filter 501 are fed to the reactive power calculating circuit 502. The

reactive power calculating circuit 502 calculates and supplies the desired amplitude of

reactive power voltage demanded by the hybrid reactive power compensation device 3.

The outputs of the second band-pass filter 501 and the reactive power calculating

circuit 502 are sent to a multiplier 503 for obtaining the first voltage control signal V<sub>1</sub>.

Page 13, amend the first full paragraph to read:

Referring again to FIGS. 4 and 5, the second voltage control signal V<sub>2</sub> is

used to regulate the voltage of the DC power capacitor 321 of the active type

reactive power compensator 32 to thereby supply a DC voltage to the power

converter 320. The active type reactive power compensator 32 has a power

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loss and thus the voltage of DC power capacitor 321 may be varied. In order maintain the active type reactive power compensator 32 operated operating normally, the DC voltage thereof must be maintained at a constant value. In 10 this condition, the active type reactive power compensator 32 must absorb/generate real power from/to the power system 1. It means that the active type reactive power compensator 32 must generate a fundamental component voltage whose phase is identical with the voltage phase of the power system 1. The hybrid reactive power compensation device 3 is adapted to provide with a reactive power and its current phase is 90 degrees leading with the fundamental component of the power system voltage. Therefore, the second voltage control signal V<sub>2</sub> is a fundamental signal leading 90 degrees with the power system voltage. The detected DC voltage of the active type reactive power compensator 32 and a preset voltage must be sent to a subtractor 504, and then the subtracted result is sent to the controller 505. The fundamental voltage of the second band-pass filter 501 derived from the power system is sent to the P-I controller 506 to thereby generate a fundamental signal leading 90 degrees. The output of the controller 505 and the output fundamental signal of the P-I controller 506 are sent to a multiplier 507 to obtain second voltage control signal V<sub>2</sub>.

#### Page 14, amend the first full paragraph to read:

Referring again to FIGS. 4 and 5, the third voltage control signal V<sub>3</sub> is used to generate a voltage equivalent to the harmonic voltage of the power system 1. The voltage of the power system 1 and the output fundamental voltage of the second bandpass filter 501 are sent to a subtractor 508 so as to obtain its harmonic component. And then the harmonic component is sent to a second amplifier 509, thereby obtaining the third voltage control signal V<sub>3</sub>. After that, the three third voltage control signals (V<sub>1</sub>, V<sub>2</sub> and V<sub>3</sub>) are add added in an adder 509 and the output of the adder 509 is passed to a second controller 510 to obtain a modulation signal. And then the modulation signal is sent to a pulse-width modulation circuit 510 to generate the pulse-width modulation

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signal and it that is sent to a driver circuit 511. Consequently, the driving signals of the power converter 320 of the active type reactive power compensator 32 can be obtained.

Page 14, amend paragraph 3 (bridging pages 14 and 15) to read:

Referring to FIG. 6, it is illustrated that the second embodiment includes the hybrid reactive power compensation device 3 of the first embodiment and an automatic power factor regulator system (APFR system) 6 connected parallel thereto. The connected hybrid reactive power compensation device 3 and APFR system 6 is are parallel connected between the power system 1 and the load 4. The power system 1 supplies the AC power to the load 4. The combination of the hybrid reactive power compensation device 3 and the APFR system 6 is used to supply the reactive power for compensating the reactive power demanded by the load 4. The APFR system 6 adjusts the reactive power step by step for rough tuning, and the hybrid reactive power compensation device 3 adjusts the reactive power linearly for fine tuning so—that improves to improve the input power factor to be elosed close to unity. Thus the capacity of the hybrid reactive power compensation device 3 is reduced. Consequently, the second embodiment merely requires a relatively small capacity of the hybrid reactive power compensation device 3 to incorporate into the APFR system 6 and it can linearly adjust the reactive power for improving the power factor.

Page 15, amend paragraph 1 (bridging pages 15 and 16) to read:

Referring to FIG. 7, it is illustrated that the hybrid reactive power compensation device 3 of the third embodiment is parallel connected between the power system 1 and the load 4. The power system 1 supplies an AC power to the load 4. The hybrid reactive power compensation device 3 is used to supply the reactive power demanded by the load 4. The hybrid reactive power compensation device 3 improves the input power factor to be elosed close to unity. The hybrid reactive power compensation device 3 includes a passive type reactive power

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compensator 31 and an active type reactive power compensator 32 serially connected thereto. The passive type reactive power compensator 31 may be a thyristor switch assembly 310 and an AC power capacitor assembly 311 serially connected thereto to form a Thyristor Switch Capacitor (TSC). In practical application, the hybrid reactive power compensation device 3 can be operated with different step numbers of the AC power capacitor 311 therein by means of switching the thyristor switch assembly 310 that accomplishes rough tuning for adjusting reactive power. Moreover, it can adjust the reactive power for fine-tuning by means of the active type reactive power compensator 32 that improves the input power factor to be elosed close to unity. The active type reactive power compensator 32 applies a control method of the first embodiment that generates the current with a fundamental waveform. Consequently, the AC power capacitor assembly 311 formed in the passive type reactive power compensator 31 can avoid the destruction caused by the power resonance.